

**Sirindhorn International Institute of Technology**  
**Thammasat University**  
 School of Information, Computer and Communication Technology

# ECS 445: Mobile Communications

## Fourier Transform and Communication Systems

Prapun Suksompong, Ph.D.  
 prapun@siit.tu.ac.th

October 29, 2009

Communication systems are usually viewed and analyzed in frequency domain. This note reviews some basic properties of Fourier transform and introduce basic communication systems.

### Contents

<b>1</b>	<b>Introduction to Signals</b>	<b>2</b>
1.1	Dirac Delta Function . . . . .	2
1.2	Fourier Series . . . . .	3
1.3	Fourier series expansion for real valued function . . . . .	5
1.4	Continuous-Time Fourier transform . . . . .	6
<b>2</b>	<b>Energy Signal and Power Signal</b>	<b>11</b>
2.1	Energy Signal . . . . .	12
2.2	Power Signal . . . . .	13
<b>3</b>	<b>Modulation</b>	<b>14</b>
<b>4</b>	<b>Sampling Theorem</b>	<b>18</b>
<b>A</b>	<b>Trig Identities</b>	<b>20</b>

# 1 Introduction to Signals

## 1.1 Dirac Delta Function

The (Dirac) delta function or (unit) impulse function is denoted by  $\delta(t)$ . It is usually depicted as a vertical arrow at the origin. Note that  $\delta(t)$  is not a true function; it is undefined at  $t = 0$ . We define  $\delta(t)$  as a generalized function which satisfies the sampling property (or sifting property)

$$\int \phi(t)\delta(t)dt = \phi(0)$$

for any function  $\phi(t)$  which is continuous at  $t = 0$ . From this definition, It follows that

$$(\delta * \phi)(t) = (\phi * \delta)(t) = \int \phi(\tau)\delta(t - \tau)d\tau = \phi(t)$$

where we assume that  $\phi$  is continuous at  $t$ . Intuitively we may visualize  $\delta(t)$  as an infinitely tall, infinitely narrow rectangular pulse of unit area:  $\lim_{\epsilon \rightarrow 0} \frac{1}{\epsilon} 1_{[|t| \leq \frac{\epsilon}{2}]}$ .

We list some interesting properties of  $\delta(t)$  here.

- $\delta(t) = 0$  when  $t \neq 0$ .  
 $\delta(t - T) = 0$  for  $t \neq T$ .
- $\int_A \delta(t)dt = 1_A(0)$ .
  - (a)  $\int \delta(t)dt = 1$ .
  - (b)  $\int_{\{0\}} \delta(t)dt = 1$ .
  - (c)  $\int_{-\infty}^x \delta(t)dt = 1_{[0, \infty)}(x)$ . Hence, we may think of  $\delta(t)$  as the “derivative” of the unit step function  $U(t) = 1_{[0, \infty)}(x)$ .
- $\int \phi(t)\delta(t)dt = \phi(0)$  for  $\phi$  continuous at 0.
- $\int \phi(t)\delta(t - T)dt = \phi(T)$  for  $\phi$  continuous at  $T$ . In fact, for any  $\epsilon > 0$ ,

$$\int_{T-\epsilon}^{T+\epsilon} \phi(t)\delta(t - T)dt = \phi(T).$$

- $\delta(at) = \frac{1}{|a|}\delta(t)$ . In particular,

$$\delta(\omega - \omega_0) = \delta(2\pi f - 2\pi f_0) = \frac{1}{2\pi}\delta(f - f_0)$$

when  $\omega = 2\pi f$  and  $\omega_0 = 2\pi f_0$ .

- $\delta(t - t_1) * \delta(t - t_2) = \delta(t - (t_1 + t_2))$ .
- $g(t) * \delta(t - t_0) = g(t - t_0)$ .
- Fourier properties:

- Fourier series:  $\delta(x - a) = \frac{1}{2\pi} + \frac{1}{\pi} \sum_{k=1}^{\infty} \cos(k(x - a))$  on  $[-\pi, \pi]$ .
- Fourier transform:  $\delta(t) = \int 1 e^{j2\pi ft} df$

- For a function  $g$  whose real-valued roots are  $t_i$ ,

$$\delta(g(t)) = \sum_{k=1}^n \frac{\delta(t - t_i)}{|g'(t_i)|} \quad (1)$$

[1, p 387]. Hence,

$$\int f(t)\delta(g(t))dt = \sum_{x:g(x)=0} \frac{f(x)}{|g'(x)|}. \quad (2)$$

Note that the (Dirac) delta function is to be distinguished from the *discrete time Kronecker* delta function.

As a finite measure,  $\delta$  is a unit mass at 0; that is for any set  $A$ , we have  $\delta(A) = 1[0 \in A]$ . In which case, we have again  $\int g d\delta = \int f(x)\delta(dx) = g(0)$  for any measurable  $g$ .

For a function  $g : D \rightarrow \mathbb{R}^n$  where  $D \subset \mathbb{R}^n$ ,

$$\delta(g(x)) = \sum_{z:g(z)=0} \frac{\delta(x - z)}{|\det dg(z)|} \quad (3)$$

[1, p 387].

## 1.2 Fourier Series

Let the (real or complex) signal  $r(t)$  be a *periodic* signal with period  $T_0$ . Suppose the following *Dirichlet* conditions are satisfied

- (a)  $r(t)$  is absolutely integrable over its period; i.e.,  $\int_0^{T_0} |r(t)| dt < \infty$ .
- (b) The number of maxima and minima of  $r(t)$  in each period is finite.
- (c) The number of discontinuities of  $r(t)$  in each period is finite.

Then  $r(t)$  can be expanded in terms of the complex exponential signals  $(e^{jn\omega_0 t})_{n=-\infty}^{\infty}$  as

$$\tilde{r}(t) = \sum_{n=-\infty}^{\infty} c_n e^{jn\omega_0 t} = c_0 + \sum_{k=1}^{\infty} (c_k e^{jk\omega_0 t} + c_{-k} e^{-jk\omega_0 t}) \quad (4)$$

where

$$\omega_0 = 2\pi f_0 = \frac{2\pi}{T_0},$$

$$c_k = \frac{1}{T_0} \int_{\alpha}^{\alpha+T_0} r(t) e^{-jk\omega_0 t} dt, \quad (5)$$

for some *arbitrary*  $\alpha$ . In which case,

$$\tilde{r}(t) = \begin{cases} r(t), & \text{if } r(t) \text{ is continuous at } t \\ \frac{r(t^+) + r(t^-)}{2}, & \text{if } r(t) \text{ is not continuous at } t \end{cases}$$

We give some remarks here.

- The parameter  $\alpha$  in the limits of the integration (5) is arbitrary. It can be chosen to simplify computation of the integral. We can simply write  $c_k = \frac{1}{T_0} \int_{T_0} r(t) e^{-jk\omega_0 t} dt$  to emphasize that we only need to integrate over one period of the signal; the starting point is not important.
- The coefficients  $c_k = \frac{1}{T_0} \int_{T_0} r(t) e^{-jk\omega_0 t} dt$  are called the ( $k^{\text{th}}$ ) **Fourier (series) coefficients** of (the signal)  $r(t)$ . These are, in general, complex numbers.
- $c_0 = \frac{1}{T_0} \int_{T_0} r(t) dt =$  average or DC value of  $r(t)$
- The Dirichlet conditions are only sufficient conditions for the existence of the Fourier series expansion. For some signals that do not satisfy these conditions, we can still find the Fourier series expansion.
- The quantity  $f_0 = \frac{1}{T_0}$  is called the **fundamental frequency** of the signal  $r(t)$ . The  $n$ th multiple of the fundamental frequency (for positive  $n$ 's) is called the  $n$ th **harmonic**.
- $c_k e^{jk\omega_0 t} + c_{-k} e^{-jk\omega_0 t} =$  the  $k^{\text{th}}$  **harmonic component** of  $r(t)$ .  
 $k = 1 \Rightarrow$  fundamental component of  $r(t)$ .
- Consider a restricted version  $r_{T_0}(t)$  of  $r(t)$  where we only consider  $r(t)$  for one specific period. Suppose  $r_{T_0}(t) \xrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} R_{T_0}(f)$ . Then,

$$c_k = \frac{1}{T_0} R_{T_0}(kf_0).$$

So, the Fourier coefficients are simply scaled samples of the Fourier transform.

**1.1.** Parseval's Identity:  $P_r = \frac{1}{T_0} \int_{T_0} |r(t)|^2 dt = \sum_{k=-\infty}^{\infty} |c_k|^2$

**1.2.** Real, Odd/Even properties

- If  $r(t)$  is even ( $r(-t) = r(t)$ ), then  $c_{-k} = c_k$ .
- If  $r(t)$  is odd ( $r(-t) = -r(t)$ ), then  $c_{-k} = -c_k$ .
- If  $r(t)$  is real valued and even, then so is  $c_k$  as a function of  $k$ .
- If  $r(t)$  is real-valued and odd, then  $c_k$ 's are pure imaginary and  $c_{-k} = -c_k$

### 1.3 Fourier series expansion for real valued function

Suppose  $r(t)$  in the previous section is real-valued; that is  $r^* = r$ . Then, we have  $c_{-k} = c_k^*$  and we provide here three alternative ways to represent the Fourier series expansion:

$$\tilde{r}(t) = \sum_{n=-\infty}^{\infty} c_n e^{jn\omega_0 t} = c_0 + \sum_{k=1}^{\infty} (c_k e^{jk\omega_0 t} + c_{-k} e^{-jk\omega_0 t}) \quad (6)$$

$$= c_0 + \sum_{k=1}^{\infty} (a_k \cos(k\omega_0 t)) + \sum_{k=1}^{\infty} (b_k \sin(k\omega_0 t)) \quad (7)$$

$$= c_0 + 2 \sum_{k=1}^{\infty} |c_k| \cos(k\omega_0 t + \angle c_k) \quad (8)$$

where the corresponding coefficients are obtained from

$$c_k = \frac{1}{T_0} \int_{\alpha}^{\alpha+T_0} r(t) e^{-jk\omega_0 t} dt = \frac{1}{2} (a_k - jb_k) \quad (9)$$

$$a_k = 2\text{Re}\{c_k\} = \frac{2}{T_0} \int_{T_0} r(t) \cos(k\omega_0 t) dt \quad (10)$$

$$b_k = -2\text{Im}\{c_k\} = \frac{2}{T_0} \int_{T_0} r(t) \sin(k\omega_0 t) dt \quad (11)$$

$$|c_k| = \sqrt{a_k^2 + b_k^2} \quad (12)$$

$$\angle c_k = -\arctan\left(\frac{b_k}{a_k}\right) \quad (13)$$

$$c_0 = \frac{a_0}{2} \quad (14)$$

$$(15)$$

The Parseval's identity can then be expressed as

$$P_r = \frac{1}{T_0} \int_{T_0} |r(t)|^2 dt = \sum_{k=-\infty}^{\infty} |c_k|^2 = c_0^2 + 2 \sum_{k=1}^{\infty} |c_k|^2$$

#### 1.3. Examples:

- Train of impulses:

$$\delta_{T_s}(t) = \sum_{k=-\infty}^{\infty} \delta(t - kT_0) = \frac{1}{T_0} \sum_{k=-\infty}^{\infty} e^{jk\omega_0 t} = \frac{1}{T_0} + \frac{2}{T_0} \sum_{k=1}^{\infty} \cos k\omega_0 t \quad (16)$$

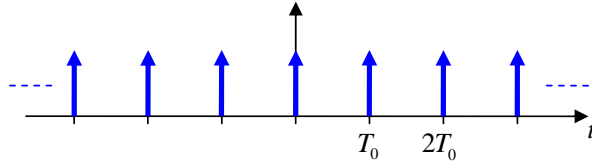


Figure 1: Train of impulses

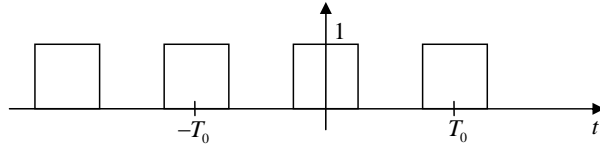


Figure 2: Square pulse periodic signal

- Square pulse periodic signal:

$$1[\cos \omega_0 t \geq 0] = \frac{1}{2} + \frac{2}{\pi} \left( \cos \omega_0 t - \frac{1}{3} \cos 3\omega_0 t + \frac{1}{5} \cos 5\omega_0 t - \frac{1}{7} \cos 7\omega_0 t + \dots \right) \quad (17)$$

We note here that multiplication by this signal is a switching function.

- Bipolar square pulse periodic signal:

$$\text{sgn}(\cos \omega_0 t) = \frac{4}{\pi} \left( \cos \omega_0 t - \frac{1}{3} \cos 3\omega_0 t + \frac{1}{5} \cos 5\omega_0 t - \frac{1}{7} \cos 7\omega_0 t + \dots \right)$$

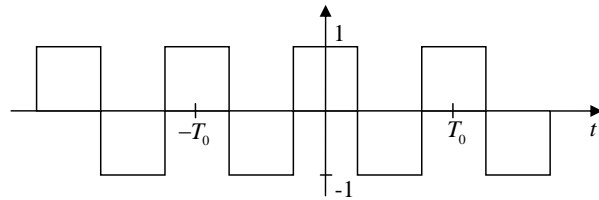


Figure 3: Bipolar square pulse periodic signal

## 1.4 Continuous-Time Fourier transform

The (direct) Fourier transform of  $g(t)$  is defined by

$$\hat{G}(\omega) = \int_{-\infty}^{\infty} g(t) e^{-j\omega t} dt. \quad (18)$$

We may simply write  $G = \mathcal{F}\{g\}$ . Sometimes the magnitude and phase of  $G$  are shown explicitly by writing  $G = |G| e^{j\theta_g}$  where both  $|G|$  and  $\theta_g$  are real-valued functions of  $\omega$ .

$$\frac{1}{2\pi} \int_{-\infty}^{\infty} \hat{G}(\omega) e^{j\omega t} d\omega = g(t) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \hat{G}(\omega) = \int_{-\infty}^{\infty} g(t) e^{-j\omega t} dt$$

In MATLAB, these identities are given by `fourier` and `ifourier`. Note also that  $\hat{G}(0) = \int g(t) dt$  and  $g(0) = \frac{1}{2\pi} \int G(\omega) dt$ .

#### 1.4. Conjugate and Time Inversion (Time Reversal):

$$\begin{aligned} g(-t) &\xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \hat{G}(-\omega) \\ g^*(t) &\xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \hat{G}^*(-\omega) \\ g^*(-t) &\xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \hat{G}^*(\omega) \end{aligned}$$

#### 1.5. Shifting properties

- Time-shift:  $g(t - t_1) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} e^{-j\omega t_1} \hat{G}(\omega)$
- Frequency-shift (or modulation):  $e^{j\omega_1 t} g(t) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \hat{G}(\omega - \omega_1)$

#### 1.6. Unit impulse:

$$e^{j\omega_0 t} \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} 2\pi \delta(\omega - \omega_0) = \delta(f - f_0) \quad (19)$$

$$\sum_{k=-\infty}^{\infty} c_k e^{jk\omega_0 t} \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \sum_{k=-\infty}^{\infty} 2\pi c_k \delta(\omega - k\omega_0) \quad (20)$$

$$\delta(t - t_0) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} e^{-j\omega t_0} \quad (21)$$

$$\delta(t) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} 1 \quad (22)$$

$$1 \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} 2\pi \delta(\omega) \quad (23)$$

$$a \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} a 2\pi \delta(\omega) \quad (24)$$

Property (20) is of importance because it shows transform of periodic signal which is expressed in its Fourier series form (as in (4)). A special case is when the signal is a train of impulses:

$$\sum_{n=-\infty}^{\infty} \delta(t - nT_0) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \omega_0 \sum_{n=-\infty}^{\infty} \delta(\omega - n\omega_0) \quad \text{where } \omega_0 = \frac{2\pi}{T_0}.$$

#### 1.7. Linearity: $c_1 g_1(t) + c_2 g_2(t) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} c_1 \hat{G}_1(\omega) + \hat{G}_2(\omega)$ .

1.8. Time-scaling rule:  $g(at) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{1}{|a|} \hat{G}\left(\frac{\omega}{a}\right)$

1.9.  $\text{Re}\{g(t)\} \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{1}{2} \left( \hat{G}(\omega) + \hat{G}^*(-\omega) \right)$

1.10. Convolution

- Convolution-in-time Rule:  $g_1(t) * g_2(t) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \hat{G}_1(\omega) \cdot \hat{G}_2(\omega)$ .

- Convolution-in-frequency Rule:  $g_1(t) \cdot g_2(t) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{1}{2\pi} \hat{G}_1(\omega) * \hat{G}_2(\omega)$ . See also (31).

1.11. Duality: Suppose  $f(t) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} g(\omega)$ . Then,  $g(t) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} 2\pi f(-\omega)$ .

1.12. Parseval's theorem:  $\int_{-\infty}^{\infty} |g(t)|^2 dt = \frac{1}{2\pi} \int_{-\infty}^{\infty} |\hat{G}(\omega)|^2 d\omega$

1.13. Unit step function:

$$u(t) = 1 [t \geq 0] \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{1}{j\omega} + \pi\delta(\omega) \quad (25)$$

$$\text{sgn } t = \begin{cases} 1, & t > 0 \\ -1, & t < 0 \end{cases} \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{2}{j\omega} \quad (26)$$

$$\frac{j}{\pi t} \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \text{sgn}(\omega) \quad (27)$$

$$(g * u)(t) = \int_{-\infty}^t g(\tau) d\tau \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{1}{j\omega} G(\omega) + \pi G(0)\delta(\omega) \quad (28)$$

So, if  $g$  (or equivalently,  $G$ ) is band-limited to  $|\omega| \leq B$ , then  $g * u$  is also bandlimited to  $|\omega| \leq B$ .

Use `heaviside` in MATLAB for  $u(t)$ . For example, (25) can be found by `syms t; fourier(heaviside(t))`.

1.14. Exponential: Assume  $\alpha, \sigma > 0$ .

$$e^{-\alpha t} u(t) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{1}{\alpha + j\omega}$$

$$e^{\alpha t} u(-t) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{1}{\alpha - j\omega}$$

$$e^{-\alpha|t|} \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{2\alpha}{\alpha^2 + \omega^2}$$

$$te^{-\alpha t} u(t) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{1}{(\alpha + j\omega)^2}$$

$$t^n e^{-\alpha t} u(t) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{n!}{(\alpha + j\omega)^{n+1}}$$

$$ke^{-\alpha t^2} \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \left( k\sqrt{\frac{\pi}{\alpha}} \right) e^{-\left(\frac{1}{4\alpha}\right)\omega^2}$$



**1.15. Modulation:**

$$\begin{aligned} \cos(\omega_c t + \theta) &\xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \pi \delta(\omega - \omega_c) e^{j\theta} + \pi \delta(\omega + \omega_c) e^{-j\theta} \\ \sin(\omega_0 t) &\xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{\pi}{j} (\delta(\omega - \omega_0) - \delta(\omega + \omega_0)) \\ g_{\omega_c, \theta}(t) = g(t) \times \cos(\omega_c t + \theta) &\xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{1}{2} \hat{G}(\omega - \omega_c) e^{j\theta} + \frac{1}{2} \hat{G}(\omega + \omega_c) e^{-j\theta} \\ g(t) \times \sin(\omega_c t + \theta) &\xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{1}{2j} \hat{G}(\omega - \omega_c) e^{j\theta} - \frac{1}{2j} \hat{G}(\omega + \omega_c) e^{-j\theta} \end{aligned}$$

Suppose  $g$  is bandlimited; that is  $G = 0$  for  $|\omega| > \omega_g = 2\pi B_g$ . If  $\omega_c > \omega_g$ , then the support sets of  $\hat{G}(\omega - \omega_c)$  and  $\hat{G}(\omega + \omega_c)$  are disjoint, and hence they are orthogonal in the frequency domain and their energy added. In which case,  $E_{g_{\omega_c, \theta}} = \frac{1}{2} E_g$ .

**1.16. Rectangular and Sinc:** Assume  $a, \omega_0 > 0$ .

$$\begin{aligned} 1[|t| \leq a] &\xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{\sin(2\pi f a)}{\pi f} = \frac{2 \sin(a\omega)}{\omega} = 2a \operatorname{sinc}(a\omega), \\ \frac{\omega_0}{\pi} \operatorname{sinc}(\omega_0 t) &= \frac{\sin(\omega_0 t)}{\pi t} \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} 1[|\omega| \leq \omega_0]. \end{aligned}$$

Note that we can get a triangle from convolution of two identical rectangular waves. In particular,

$$1[|t| \leq a] * 1[|t| \leq a] = (2a - |t|) \times 1[|t| \leq 2a].$$

Therefore,

$$\left(1 - \frac{1}{b}|t|\right) 1[|t| \leq b] \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} b \left(\frac{\sin \pi f b}{\pi f b}\right)^2.$$

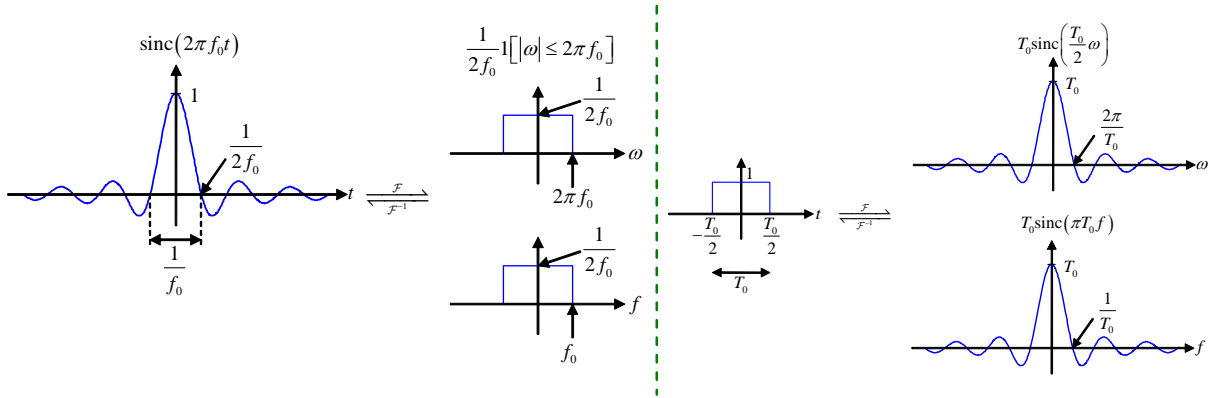


Figure 4: Fourier transform of sinc and rectangular functions

**1.17. Derivative rules:**

- Time-derivative rule:  $\frac{d}{dt}g(t) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} j\omega \hat{G}(\omega)$

- Frequency-derivative rule:  $-jtg(t) \xrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{d}{d\omega} \hat{G}(\omega)$

### 1.18. Real, Odd, and Even

- Conjugate Symmetry Property: If  $g(t)$  is real-valued ( $g(t) = g^*(t)$ ), then  $\hat{G}(-\omega) = \hat{G}^*(\omega)$ . In particular,  $|G|$  is even and  $\theta_g$  is odd.
- If  $g(t)$  is even ( $g(t) = g(-t)$ ), then  $\hat{G}(\omega)$  is also even ( $\hat{G}(-\omega) = \hat{G}(\omega)$ )
- If  $g(t)$  is odd ( $g(t) = -g(-t)$ ), then  $\hat{G}(\omega)$  is also odd ( $\hat{G}(-\omega) = -\hat{G}(\omega)$ )
- If  $g(t)$  is real and even, then so is  $\hat{G}(\omega)$ .
- If  $g(t)$  is real and odd, then  $\hat{G}(\omega)$  is pure imaginary and odd.

### 1.19. A signal cannot be simultaneously time-limited and band-limited.

*Proof.* Suppose  $g(t)$  is simultaneously (1) time-limited to  $T_0$  and (2) band-limited to  $B$ . Pick any positive number  $T_s$  and positive integer  $K$  such that  $f_s = \frac{1}{T_s} > 2B$  and  $K > \frac{T_0}{T_s}$ . The sampled signal  $g_{T_s}(t)$  is given by

$$g_{T_s}(t) = \sum_k g[k] \delta(t - kT_s) = \sum_{k=-K}^K g[k] \delta(t - kT_s)$$

where  $g[k] = g(kT_s)$ . Now, because we sample the signal faster than the Nyquist rate, we can reconstruct the signal  $g$  by producing  $g_{T_s} * h_r$  where the LPF  $h_r$  is given by

$$H_r(\omega) = T_s 1[\omega < 2\pi f_c]$$

with the restriction that  $B < f_c < \frac{1}{T_s} - B$ . In frequency domain, we have

$$G(\omega) = \sum_{k=-K}^K g[k] e^{-jk\omega T_s} H_r(\omega).$$

Consider  $\omega$  inside the interval  $I = (2\pi B, 2\pi f_c)$ . Then,

$$0 \stackrel{\omega > 2\pi B}{=} G(\omega) \stackrel{\omega < 2\pi f_c}{=} T_s \sum_{k=-K}^K g(kT_s) e^{-jk\omega T_s} \stackrel{z = e^{j\omega T_s}}{=} T_s \sum_{k=-K}^K g(kT_s) z^{-k} \quad (29)$$

Because  $z \neq 0$ , we can divide (29) by  $z^{-K}$  and then the last term becomes a polynomial of the form

$$a_{2K} z^{2K} + a_{2K-1} z^{2K-1} + \dots + a_1 z + a_0.$$

By fundamental theorem of algebra, this polynomial has only finitely many roots— that is there are only finitely many values of  $z = e^{j\omega T_s}$  which satisfies (29). Because there are uncountably many values of  $\omega$  in the interval  $I$  and hence uncountably many values of  $z = e^{j\omega T_s}$  which satisfy (29), we have a contradiction.  $\square$

**1.20.** Fourier transform of periodic signal: For any periodic signal  $r(t)$  with period  $T_0$ , using the Fourier series, we can express it as

$$\tilde{r}(t) = \sum_{n=-\infty}^{\infty} c_n e^{jn\omega_0 t} = c_0 + \sum_{k=1}^{\infty} (c_k e^{jk\omega_0 t} + c_{-k} e^{-jk\omega_0 t}), \quad (4)$$

where  $\omega_0 = 2\pi f_0 = \frac{2\pi}{T_0}$ . Hence, the Fourier transform is

$$R(f) = \sum_{n=-\infty}^{\infty} c_n \delta(f - nf_0)$$

**1.21.** Sometimes, the Fourier transform above is denoted by  $\hat{G}(\Omega)$  to distinguish it from the DTFT. In which case,

$$\frac{1}{2\pi} \int_{-\infty}^{\infty} \hat{G}(\Omega) e^{j\Omega t} d\Omega = g(t) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \hat{G}(\Omega) = \int_{-\infty}^{\infty} g(t) e^{-j\Omega t} dt.$$

Some references define

$$G(f) = \int_{-\infty}^{\infty} g(t) e^{-j2\pi f t} dt. \quad (30)$$

In which case, we have

$$\int_{-\infty}^{\infty} G(f) e^{j2\pi f t} df = g(t) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} G(f) = \int_{-\infty}^{\infty} g(t) e^{-j2\pi f t} dt.$$

This definition eliminates several extra  $\pi$  and  $2\pi$  factors in the identities resulting from the definition (18). In particular, there is no factor of  $\frac{1}{2\pi}$  in the convolution-in-frequency formula.

$$g_1(t) \cdot g_2(t) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} G_1(f) * G_2(f) \quad (31)$$

Of course, (18) and (30) are related by

$$G(f) = \hat{G}(\Omega) \Big|_{\Omega=2\pi f} \quad \text{and} \quad \hat{G}(\Omega) = G(f) \Big|_{f=\frac{\Omega}{2\pi}}.$$

## 2 Energy Signal and Power Signal

For a signal  $g(t)$ , the instantaneous power  $p(t)$  dissipated in the  $1\text{-}\Omega$  resistor is  $p_g(t) = |g(t)|^2$  regardless of whether  $g(t)$  represents a voltage or a current. To emphasize the fact that this power is based upon unity resistance, it is often referred to as the normalized power. The total energy of the signal  $g(t)$  is then

$$E_g = \int |g(t)|^2 dt$$

and the average power is given by

$$P_g = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T/2}^{T/2} |g(t)|^2 dt = \lim_{T \rightarrow \infty} \frac{1}{2T} \int_{-T}^T |g(t)|^2 dt.$$

If  $E_g$  is finite and nonzero,  $g$  is referred to as an **energy signal**. If  $p_g$  is finite and nonzero,  $g$  is referred to as a **power signal**. Note that the power signal has infinite energy and an energy signal has zero average power; thus the two categories are mutually exclusive.

## 2.1 Energy Signal

### 2.1.1 Definitions

- Energy:  $E_g = \int |g(t)|^2 dt$ .
- Energy spectral density (ESD):  $\Psi_g(\omega) = |G(\omega)|^2$ .
  - ESD is a positive, real, and even function of  $\omega$ .
- Time autocorrelation function:

$$\begin{aligned} \psi_g(\tau) &= \int g^*(\mu)g(\mu + \tau)d\mu = g^*(\tau) * g(-\tau) \\ &= \int g(\mu)g^*(\mu - \tau)d\mu = g(\tau) * g^*(-\tau) \end{aligned}$$

- $\psi_g$  is invariant to time-shift in  $g$ : Suppose  $h(t) = g(t - t_0)$ , then  $\psi_g = \psi_h$ .

### 2.2.

$$\begin{aligned} E_g &= \int |g(t)|^2 dt \\ &= \frac{1}{2\pi} \int |G(\omega)|^2 d\omega = \frac{1}{2\pi} \int \Psi_g(\omega)d\omega = \int \Psi_g(2\pi f)df \end{aligned}$$

### 2.3. $\psi_g(\tau) \xrightarrow{\mathcal{F}} \Psi_g(\omega)$

### 2.4. Example

- For  $g(t) = 1_{[t_0, t_0+T]}(t)$ , we have  $\psi_g(\tau) = \left(1 - \frac{|\tau|}{T}\right) 1_{[-T, T]}(\tau)$  and  $\Psi_g(\omega) = T \operatorname{sinc}^2\left(\frac{\omega T}{2}\right)$ .

**2.5.** Suppose  $g$  and  $y$  are the input and output signals of an LTI system with transfer function  $H$  ( $g \rightarrow \boxed{\text{LTI} : H} \rightarrow y$ ), then  $\Psi_y(\omega) = |H(\omega)|^2 \Psi_g(\omega)$ .

## 2.2 Power Signal

### 2.6. Definitions:

- $g_T(t) = g(t) \mathbb{1} \left[ |t| \leq \frac{T}{2} \right]$
- Power:  $P_g = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T/2}^{T/2} |g(t)|^2 dt = \lim_{T \rightarrow \infty} \frac{1}{T} E_{g_T} = \langle g^2 \rangle$ .
- Power spectral density (PSD):  $S_g(\omega) = \lim_{T \rightarrow \infty} \frac{1}{T} |G_T(\omega)|^2 = \lim_{T \rightarrow \infty} \frac{1}{T} \Psi_{g_T}^2(t)$ 
  - PSD represents the power per unit bandwidth (in Hz) of the spectral components at the frequency  $\omega$ .
  - PSD is a positive, real, and even function of  $\omega$ .
- Time autocorrelation function:

$$\begin{aligned} R_g(\tau) &= \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T/2}^{T/2} g^*(\mu) g(\mu + \tau) d\mu = \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T/2}^{T/2} g(\mu) g^*(\mu - \tau) d\mu \\ &= \langle g^*(\cdot) g(\cdot + \tau) \rangle = \langle g(\cdot) g^*(\cdot - \tau) \rangle \end{aligned}$$

- $R_g(-\tau) = R_g^*(\tau)$

### 2.7.

$$\begin{aligned} P_g &= \lim_{T \rightarrow \infty} \frac{1}{T} \int_{-T/2}^{T/2} |g(t)|^2 dt = \lim_{T \rightarrow \infty} \frac{1}{T} E_{g_T} = \langle g^2 \rangle \\ &= \frac{1}{2\pi} \int S_g(\omega) d\omega = \int S_g(2\pi f) df \end{aligned}$$

### 2.8. $R_g(\tau) \xrightarrow{\mathcal{F}} S_g(\omega)$

### 2.9. $R_{g_1 g_2}(\tau) = \lim_{T \rightarrow \infty} \int_{-T/2}^{T/2} g_1(t) g_2(t + \tau) dt$

- If  $g = g_1 + g_2$ , then  $R_g = R_{g_1} + R_{g_2} + R_{g_1 g_2} + R_{g_2 g_1}$ .

### 2.10. Examples

- $g(t) = a \cos(\omega_0 t + \theta)$ 
  - $R_g(\tau) = \frac{1}{2} a^2 \cos \omega_0 \tau$
  - $S_g(\omega) = \frac{\pi}{2} a^2 (\delta(\omega - \omega_0) + \delta(\omega + \omega_0))$
- Periodic function  $r(t) = d_0 + \sum_{n=1}^{\infty} d_n \cos(n\omega_0 t + \theta_n)$ 
  - $R_r(\tau) = d_0^2 + \frac{1}{2} \sum_{n=1}^{\infty} d_n^2 \cos n\omega_0 \tau$
  - $S_r(\omega) = 2\pi d_0^2 \delta(\omega) + \frac{\pi}{2} \sum_{n=1}^{\infty} d_n^2 (\delta(\omega - n\omega_0) + \delta(\omega + n\omega_0))$

**2.11.** Suppose  $g$  and  $y$  are the input and output signals of an LTI system with transfer function  $H$  ( $g \rightarrow \boxed{\text{LTI} : H} \rightarrow y$ ), then  $S_y(\omega) = |H(\omega)|^2 S_g(\omega)$ .

### 3 Modulation

Let the *carrier frequency* be at  $f_c$  [Hz] with corresponding angular frequency  $\omega_c = 2\pi f_c$ .

#### 3.1. Double-sideband suppressed carrier (DSB-SC) modulation:

- (a) See Figure 6.
- (b) Modulation
  - (i) Modulated signal:  $x(t) = m(t) \cos \omega_c t$
  - (ii) Recall from (1.15) that

$$g_{\omega_c, \theta}(t) = g(t) \times \cos(\omega_c t + \theta) \xleftrightarrow[\mathcal{F}^{-1}]{\mathcal{F}} \frac{1}{2} \hat{G}(\omega - \omega_c) e^{j\theta} + \frac{1}{2} \hat{G}(\omega + \omega_c) e^{-j\theta}.$$

Furthermore, if (1)  $g$  is bandlimited to  $|\omega| \leq \omega_g = 2\pi B_g$  and (2)  $|\omega| > \omega_g = 2\pi B_g$ , then  $E_{g_{\omega_c, \theta}} = \frac{1}{2} E_g$ . This is not true for non-bandlimited  $g$ . For example, take  $g = 1_{[0, T]}$ , then

$$\int g^2(t) \cos^2(\omega_c t) dt = \frac{E_g}{2} + \frac{1}{2\omega} \cos(\omega_c T) \sin(\omega_c T)$$

where the second term does not vanish for all  $\omega_c$ . It will vanish when  $\omega_c \rightarrow \infty$ .

- (iii) To produce the modulated signal  $m(t) \cos \omega_c t$ , we may use the following methods which generate the modulated signal along with other signals which can be eliminated by a bandpass filter restricting frequency contents to around  $\omega_c$ .
  - i. When it is easier to build a squarer than a multiplier, use

$$\begin{aligned} (m(t) + c \cos(\omega_c t))^2 &= m^2(t) + c^2 \cos^2(\omega_c t) + 2cm(t) \cos(\omega_c t) \\ &= m^2(t) + \frac{c^2}{2} + 2cm(t) \cos(\omega_c t) + \frac{c^2}{2} \cos(2\omega_c t). \end{aligned}$$

Alternative, can use  $(m(t) + c \cos(\frac{\omega_c t}{2}))^3$ .

- ii. Multiply  $m(t)$  by “any” periodic and even signal  $r(t)$  whose period is  $T_c = \frac{2\pi}{\omega_c}$ . Because  $r(t)$  is an even function, we know that

$$r(t) = c_0 + \sum_{k=1}^{\infty} a_k \cos(k\omega_c t).$$

Therefore,

$$m(t)r(t) = c_0 m(t) + \sum_{k=1}^{\infty} a_k m(t) \cos(k\omega_c t).$$

See also [2, p 157]. In general, for this scheme to work, we need

- $a_1 \neq 0$ ; that is  $T_c$  is the “least” period of  $r$ ;
- $\omega_c > 4\pi B$ ; that is  $f_c > 2B$  (to prevent overlapping).

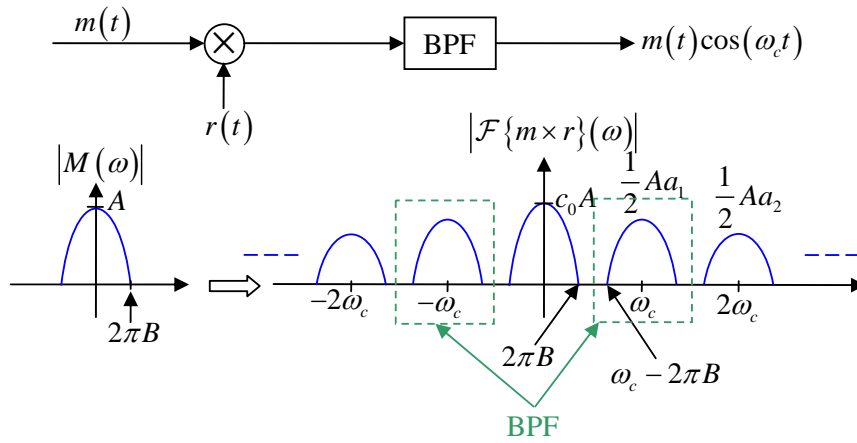


Figure 5: Modulation of  $m(t)$  via even and periodic  $r(t)$

Note that if  $r(t)$  is not even, then by (8), the outputted modulated signal is of the form  $a_1 m(t) \cos(\omega_c t + \phi_1)$ .

- iii. **Switching modulator**: set  $r(t)$  to be the square pulse train given by (17). Multiplying this  $r(t)$  to the signal  $m(t)$  is equivalent to switching  $m(t)$  on and off periodically.

It is equivalent to periodically turning the switch on (letting  $m(t)$  pass through) for half a period  $T_c = \frac{1}{f_c}$ .

- (iv) Need  $\omega_c \geq 2\pi B$

- (v) The modulated signal spectrum centered at  $\omega_c$  is composed of two parts: a portion that lies above  $\omega_c$ , known as the upper sideband (USB), and a portion that lies below  $\omega_c$ , known as the lower sideband (LSB). Hence, this is a modulation scheme with double sidebands.

- (vi) The modulated signal does not contain a discrete component of the carrier frequency  $\omega_c$ .

(c) Demodulation:

- (i) Basic idea:

$$\text{LPF} \left\{ \left( m(t) \sqrt{2} \cos \omega_c t \right) \sqrt{2} \cos ((\omega_c + \Delta\omega)t + \theta) \right\} = m(t) \cos ((\Delta\omega)t + \theta).$$

Of course, we want  $\Delta\omega = 0$  and  $\theta = 0$ ; that is the receiver must generate a carrier in phase and frequency synchronism with the incoming carrier. These demodulators are called **synchronous** or **coherent** (also **homodyne**) demodulator [2, p 161].

- (ii) Suppose the propagation time is  $\tau$ , then we have

$$\text{LPF} \left\{ \left( m(t - \tau) \sqrt{2} \cos (\omega_c (t - \tau)) \right) \sqrt{2} \cos (\omega_c (t - \mu)) \right\} = m(t - \tau) \cos (\omega_c (\tau - \mu))$$

At the receiver, we want  $\mu = \tau$ .

- (iii) **Envelope detector.** See [2, p 168]. Note that this method need  $m(t) \geq 0$ .  
 (iv) **Switching Demodulator:**

$$\text{LPF}\{m(t) \cos(\omega_c t) \times 1[\cos(\omega_c t) \geq 0]\} = \frac{1}{\pi}m(t) \quad (32)$$

[2, p 162].

- (v) **Rectifier Detector:** Suppress the negative part of  $m(t)\cos(\omega_c t)$  using a diode. This is equivalent to switching demodulator in (32). It is in effect synchronous detection performed without using a local carrier [2, p 167].

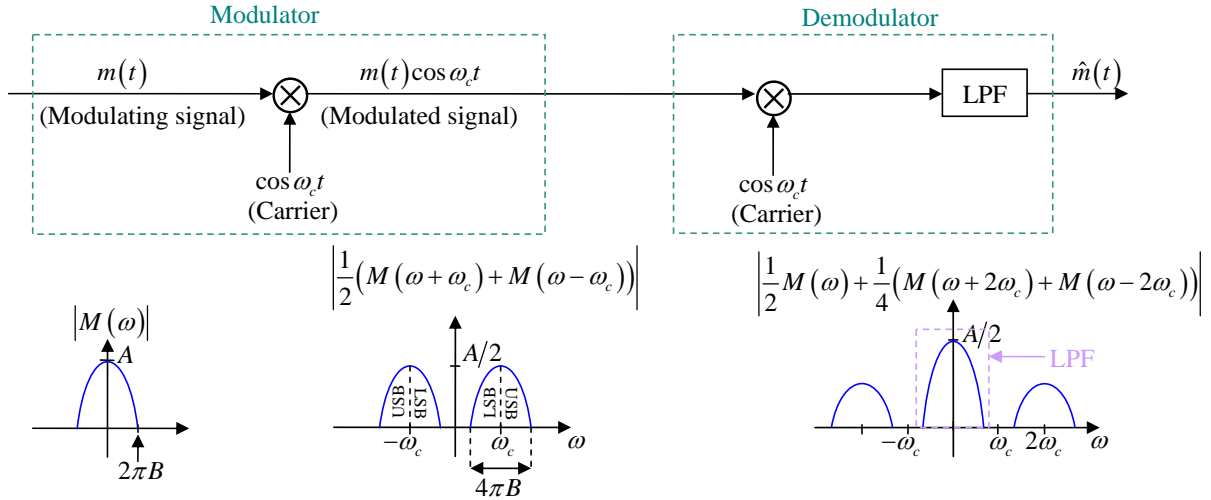


Figure 6: DSB-SC modulation and demodulation

### 3.2. Amplitude Modulation (AM):

$$\varphi_{\text{AM}}(t) = (A + m(t)) \cos \omega_c t = \underbrace{A \cos \omega_c t}_{\text{carrier}} + \underbrace{m(t) \cos \omega_c t}_{\text{sidebands}}$$

### 3.3. Quadrature amplitude modulation (QAM):

$$\varphi_{\text{QAM}}(t) = m_1(t) \cos(\omega_c t) + m_2(t) \sin(\omega_c t)$$

$$\text{LPF}\{\varphi_{\text{QAM}}(t) 2 \cos((\omega_c + \Delta\omega)t + \delta)\} = m_1(t) \cos((\Delta\omega)t + \delta) - m_2(t) \sin((\Delta\omega)t + \delta)$$

$$\text{LPF}\{\varphi_{\text{QAM}}(t) 2 \sin((\omega_c + \Delta\omega)t + \delta)\} = m_1(t) \sin((\Delta\omega)t + \delta) + m_2(t) \cos((\Delta\omega)t + \delta)$$

**Definition 3.4** (Instantaneous frequency). Consider a **generalized sinusoidal** signal

$$x(t) = A \cos \theta(t)$$

where  $\theta(t)$  is the **generalized angle**.



- The generalized angle for conventional sinusoid is  $\omega_c t + \theta_0$ .

Define the **instantaneous frequency**  $\omega_i$  at  $t$  to be the slope of  $\theta(t)$  at  $t$ ; that is

$$\omega_i(t) = \frac{d}{dt}\theta(t).$$

Therefore,

$$\theta(t) = \int_{-\infty}^t \omega_i(\tau) d\tau. \quad (33)$$

- It is tempting to use  $\tilde{x}(t) = A \cos(\omega_i(t)t + \theta_0)$  instead of  $A \cos \theta(t)$  given by (33). The idea is that we replace the frequency term in the standard sinusoid with the instantaneous frequency. This can lead to very different results. In particular, the instantaneous frequency of  $\tilde{x}$  is  $\omega_i(t) + \omega_i'(t)t \neq \omega_i(t)$ .

For example, suppose the instantaneous frequency is given by  $\omega_i(t) = t$ . Then, the instantaneous frequency of  $\tilde{x}$  is  $2t$  which doubles the desired frequency.

Figure 7: Comparison between  $\tilde{x}(t) = \cos(t \times t)$  and  $x(t) = \cos\left(\int_0^t \tau d\tau\right)$ . The “frequencies” at  $t = 5$  of  $x$  and  $\tilde{x}$  are 5 and 10, respectively.

### 3.5. Angle modulation (or exponential modulation)

(a) **Generalized angle modulation:**

$$\varphi(t) = A \cos(\omega_c t + \theta_0 + (m * h)(t))$$

where  $h$  is causal.

(b) **Frequency modulation (FM):**

$$\varphi_{\text{FM}}(t) = A \cos\left(\omega_c t + \theta_0 + k_f \int_{-\infty}^t m(\tau) d\tau\right).$$

- The instantaneous frequency is given by

$$\omega_i(t) = \omega_c + k_f m(t).$$

- $h(t) = k_f 1_{[0, \infty)}(t)$
- The BW is  $\approx 2k_f m_p$  where  $m_p$  is the peak amplitude of  $m(t)$ .

(c) **Phase modulation (PM):**

$$\varphi_{\text{PM}}(t) = A \cos(\omega_c t + \theta_0 + k_p m(t))$$

- $h(t) = k_p \delta(t)$ .
- PM is actually the FM when modulating signal is  $m'(t)$ .
- The BW is  $\approx 2k_f m'_p$  where  $m'_p$  is the peak amplitude of  $m'(t)$ . (To see this, use the above observation and the approximation for the BW of FM.)

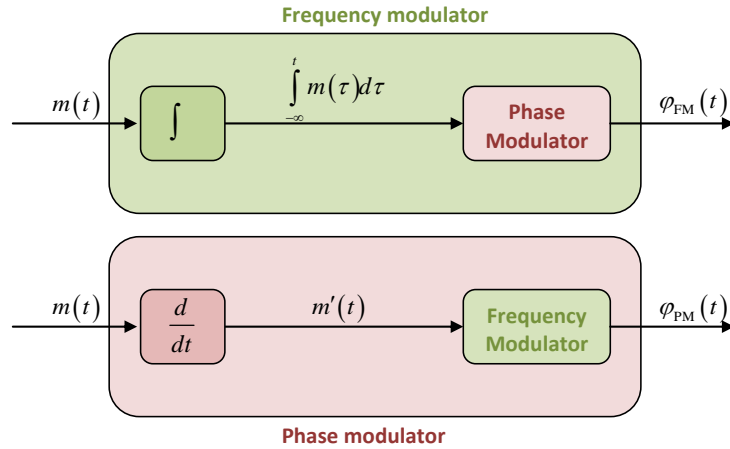


Figure 8: PM and FM are inseparable [2, Fig 5.2].

## 4 Sampling Theorem

A low-pass signal  $g$  whose spectrum is band-limited to  $B$  Hz ( $G(\omega) = 0$  for  $|\omega| > 2\pi B$ ) can be reconstructed exactly (without any error) from its sample taken uniformly at a rate (sampling frequency)  $R_s > 2B$  Hz (samples per second).

4.1. The “sampling” can be done by producing

$$g_{T_s}(t) = g(t) r_{T_s}(t)$$

where  $r_{T_s}$

- (a) is periodic with period  $T_s = \frac{1}{R_s} < \frac{1}{2B}$
- (b) has nonzero mean.

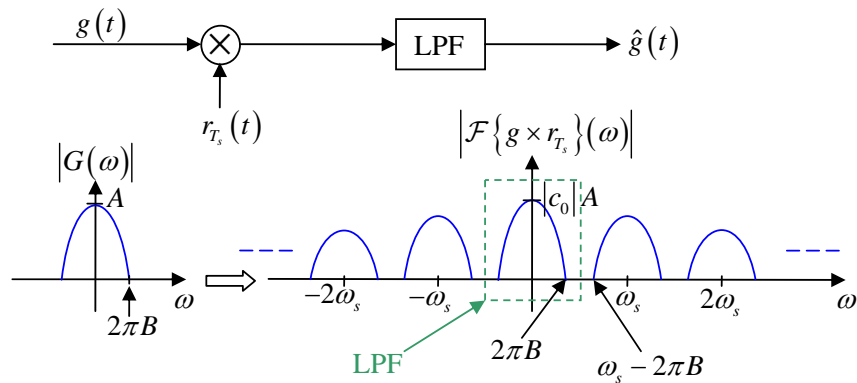


Figure 9: Sampling and Reconstruction

**4.2. Signal Reconstruction:** Because  $r_{T_s}$  is periodic, it has fourier series expansion

$$\tilde{r}(t) = \sum_{n=-\infty}^{\infty} c_n e^{jn\omega_0 t}$$

where  $\omega_s = 2\pi f_s = \frac{2\pi}{T_s}$ . Hence,

$$G_{T_s}(\omega) = \sum_n c_n G(\omega - n\omega_s).$$

Suppose  $2\pi B < \omega_s - 2\pi B$  (or equivalently  $R_s > 2B$ ), then there is no overlapping and we can get  $G$  back by LPF  $H$  with cutoff  $f_c \in [B, R_s - B)$ . More specifically,

$$H(\omega) = \frac{1}{c_0} 1[|\omega| \leq \omega_c] \xleftrightarrow[\mathcal{F}]{\mathcal{F}^{-1}} h(t) = \frac{\omega_c}{c_0 \pi} \text{sinc}(\omega_c t) = \frac{2f_c}{c_0} \text{sinc}(2\pi f_c t).$$

**4.3. Interpolation formula:** Suppose  $r_{T_s}$  is a train of impulses  $\delta_{T_s}$  as in (16). In which case,

$$g_{T_s}(t) = \sum_k g[k] \delta(t - kT_s)$$

where  $g[k] = g(kT_s)$ . Note that we have  $c_0 = \frac{1}{T_s} = f_s$ . Therefore,

$$H(\omega) = T_s 1[|\omega| \leq \omega_c] \xleftrightarrow[\mathcal{F}]{\mathcal{F}^{-1}} h(t) = \frac{2f_c}{f_s} \text{sinc}(2\pi f_c t).$$

The filtered output  $\hat{g} = g_{T_s} * h$  which is  $g$  can now be expressed as a sum

$$g(t) = \sum_k g[k] h(t - kT_s) = \frac{2f_c}{f_s} \sum_k g[k] \text{sinc}(2\pi f_c (t - kT_s))$$

Furthermore, suppose we choose  $f_s = 2B$  and  $f_c = B$ , then we have

$$H(\omega) = \frac{1}{2B} 1[|\omega| \leq 2\pi B] \xleftrightarrow[\mathcal{F}]{\mathcal{F}^{-1}} h(t) = \text{sinc}(2\pi B t).$$

In which case,

$$g(t) = \sum_k g[k] \text{sinc}(2\pi B (t - kT_s)) = \sum_k g[k] \text{sinc}(2\pi B t - k\pi).$$

**4.4.** A band pass signal whose spectrum exists over a frequency band  $f_c - \frac{B}{2} < |f| < f_c + \frac{B}{2}$  has a bandwidth  $B$  Hz. Such a signal is uniquely determined by  $2B$  samples per second. The sampling scheme uses two interlaced sampling trains, each at a rate of  $B$  samples per second (known as second-order sampling).

# A Trig Identities

## A.1. Cosine function

(a) Is an even function:  $\cos(-x) = \cos(x)$ .

(b)  $\cos\left(x - \frac{\pi}{2}\right) = \sin(x)$ .

(c) Sum formula:

$$\cos(x \pm y) = \cos x \cos y \mp \sin x \sin y. \quad (34)$$

(d) Product-to-Sum Formula:

$$\cos(x) \cos(y) = \frac{1}{2} (\cos(x + y) + \cos(x - y)).$$

$$(e) \cos^n x = \begin{cases} \frac{1}{2^{n-1}} \sum_{k=0}^{\frac{n-1}{2}} \binom{n}{k} \cos((n-2k)x), & \text{odd } n \geq 1 \\ \frac{1}{2^n} \left( \sum_{k=0}^{\frac{n}{2}-1} 2 \binom{n}{k} \cos((n-2k)x) + \binom{n}{\frac{n}{2}} \right), & \text{even } n \geq 2 \end{cases}$$

(f) Any two real numbers  $a, b$  can be expressed in terms of cosine and sine with the same amplitude and phase:

$$(a, b) = (A \cos(\phi), A \sin(\phi)), \quad (35)$$

where  $A = \sqrt{a^2 + b^2}$  and  $\phi = \tan^{-1} \frac{b}{a}$ . This is simply the polar-coordinates from of point  $(a, b)$  on Cartesian coordinates.

## A.2. Properties of $e^{ix}$

(a) **Euler's formula:**  $e^{ix} = \cos x + i \sin x$ . Hence,

$$\cos(A) = \operatorname{Re}(e^{jA}) = \frac{1}{2} (e^{jA} + e^{-jA})$$

$$\sin(A) = \operatorname{Im}(e^{jA}) = \operatorname{Re}(-je^{jA}) = \operatorname{Re}\left(-\frac{1}{j}e^{jA}\right) = \frac{1}{2j} (e^{jA} - e^{-jA}).$$

- We can use  $\cos x = \frac{1}{2} (e^{ix} + e^{-ix})$  and  $\sin x = \frac{1}{2i} (e^{ix} - e^{-ix})$  to derive many trigonometric identities.

In fact, we can combine linear combination of cosine and sine of the same argument into a single cosine by

$$A \cos \omega_0 t + B \sin \omega_0 t = \sqrt{A^2 + B^2} \cos\left(\omega_0 t - \tan^{-1} \frac{B}{A}\right).$$

To see this, note that

$$\begin{aligned} A \cos \omega_0 t + B \sin \omega_0 t &= \operatorname{Re}(Ae^{j\omega_0 t}) + \operatorname{Re}(-jBe^{j\omega_0 t}) = \operatorname{Re}((A - jB)e^{j\omega_0 t}) \\ &= \operatorname{Re}\left(\sqrt{A^2 + B^2} e^{-j \tan^{-1} \frac{B}{A}} e^{j\omega_0 t}\right). \end{aligned}$$

Another way to see this is to reexpress the two real numbers  $A, B$  using (35) and then use (34).

(b)  $e^{jx}$  is periodic with period  $2\pi$ .

(c) Any complex number  $z = x + jy$  can be expressed as  $z = \sqrt{x^2 + y^2} e^{j \tan^{-1}(\frac{y}{x})} = |z| e^{j\phi}$ .

- $z^t = |z|^t e^{j\phi t}$ .

(d) More relationship with sin and cos.

- $e^{jAt} + e^{jBt} = 2e^{j\frac{A+B}{2}t} \cos\left(\frac{A-B}{2}\right)$ .
- $e^{jAt} - e^{jBt} = 2je^{j\frac{A+B}{2}t} \sin\left(\frac{A-B}{2}\right)$
- $\frac{e^{jAt} - e^{jBt}}{e^{jCt} - e^{jDt}} = e^{j\frac{(A+B)-(C+D)}{2}t} \frac{\sin\left(\frac{A-B}{2}\right)}{\sin\left(\frac{C-D}{2}\right)}$ .

## References

- [1] Donald G. Childers. *Probability And Random Processes Using MATLAB*. McGraw-Hill, 1997. 1.1, 1.1
- [2] B. P. Lathi. *Modern Digital and Analog Communication Systems*. Oxford University Press, 1998. 2(c)ii, 3a, 3c, 3d, 3e, 8
- [3] C. Britton Rorabaugh. *Communications Formulas and Algorithms: For System Analysis and Design*. McGraw-Hill, 1990.