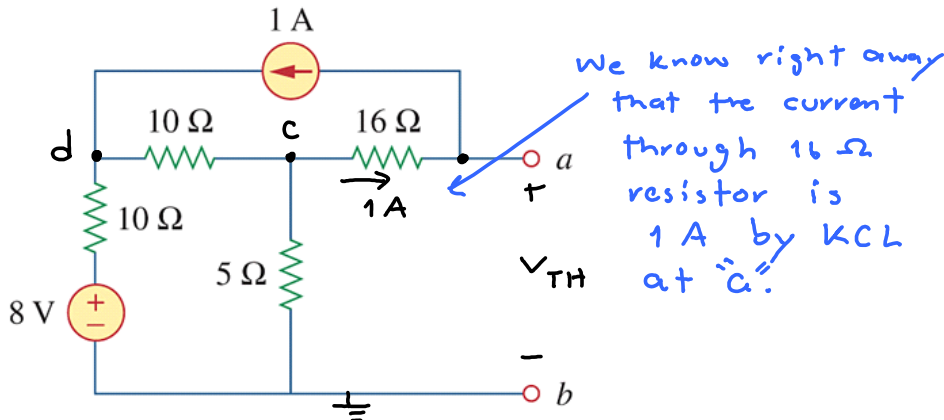


4.39 First we find V_{TH}



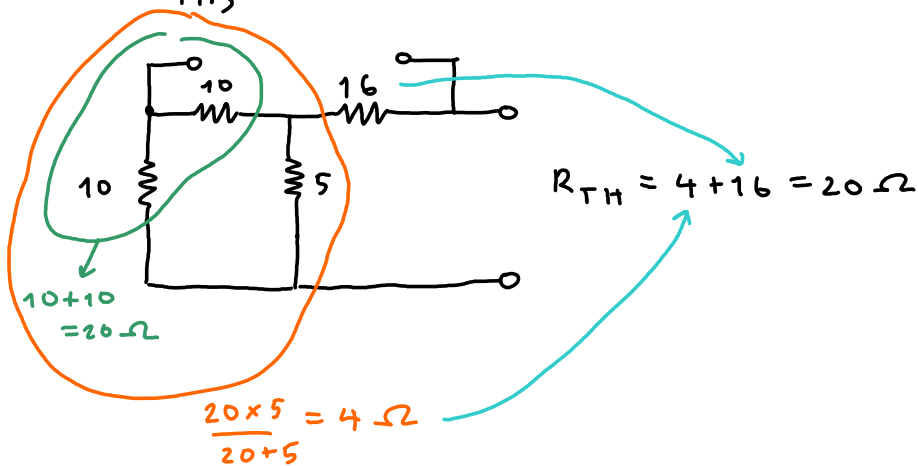
Use nodal analysis:

$$\left. \begin{aligned} 1 + \frac{V_c - V_d}{10} + \frac{V_c}{5} &= 0 \\ \frac{V_d - 8}{10} + \frac{V_d - V_c}{10} - 1 &= 0 \end{aligned} \right\} \Rightarrow \begin{aligned} V_c &= -\frac{2}{5} \\ V_d &= \frac{44}{5} \end{aligned}$$

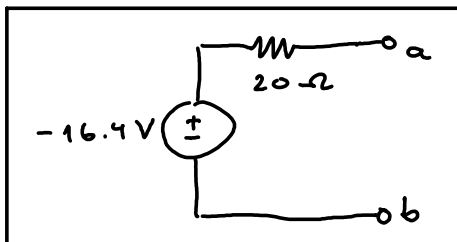
Maple

$$V_a = V_c - 16 \times 1 = -\frac{2}{5} - 16 = -16.4 \text{ V} = V_{TH}$$

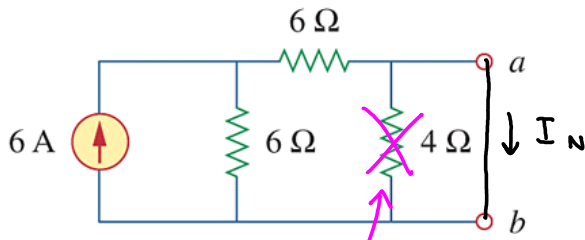
For R_{TH} , we deactivate all the sources:



The Thevenin equivalent at terminal a-b is



4.45 I_N = short-circuit current

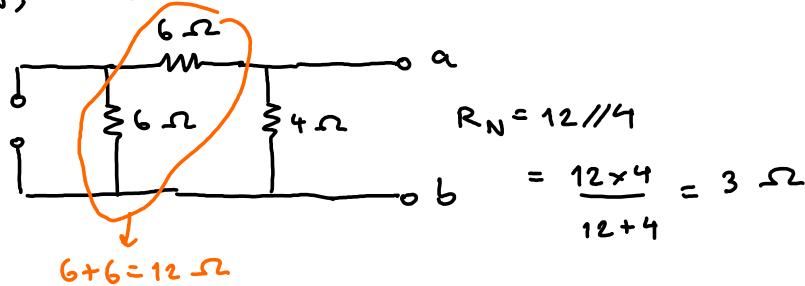


The $4\ \Omega$ resistor is gone because it is short out.

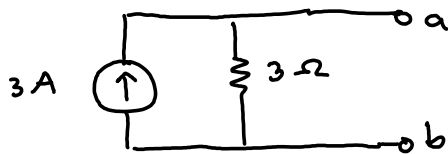
By the current divider formula, the 6A from the current source is split equally between the two $6\ \Omega$ resistors.

Hence, $I_N = 3\text{ A}$.

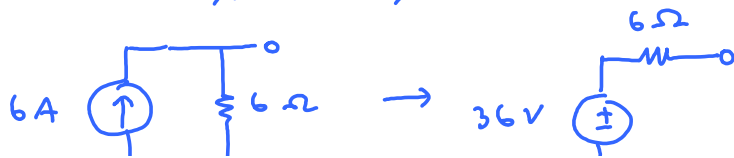
For R_N , we deactivate all the sources:

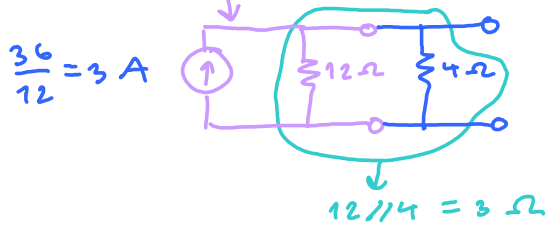
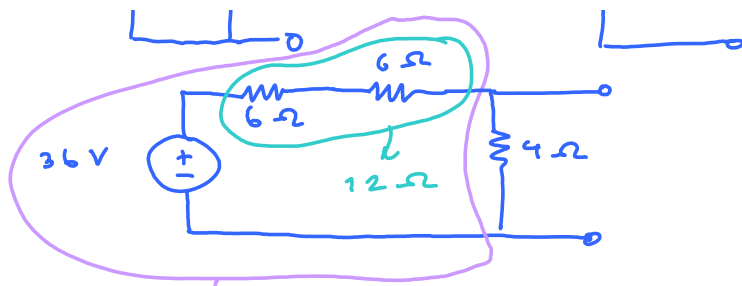


The Norton equivalent is given by

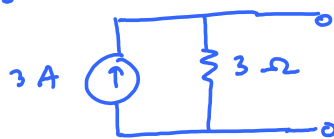


Alternatively, we may use source transformation



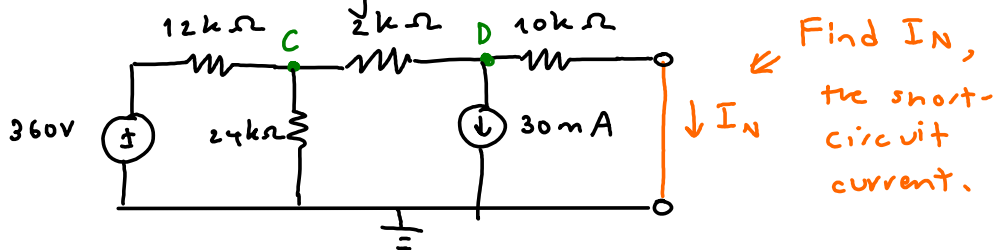


This gives



which is the same as what we got from Norton's theorem above.

4.56) Note that the question specifies that we have to use the Norton theorem. Hence we will first need to find Norton equivalent of the following circuit



Find I_N , the short-circuit current.

Use Nodal analysis:

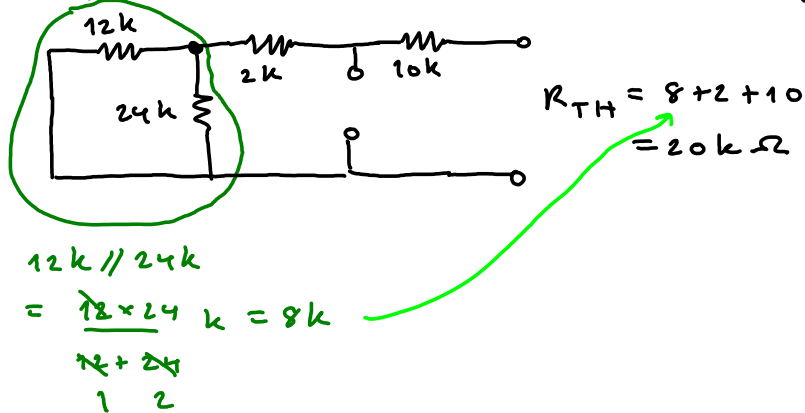
$$\left. \begin{aligned} \text{At } c: \quad \frac{V_c - 360}{12k} + \frac{V_c}{24k} + \frac{V_c - V_D}{2k} &= 0 \\ 30m + \frac{V_D - V_c}{2k} + \frac{V_D}{10k} &= 0 \end{aligned} \right\} \Rightarrow \begin{aligned} V_c &= 24V \\ V_D &= -30V \end{aligned}$$

Note that

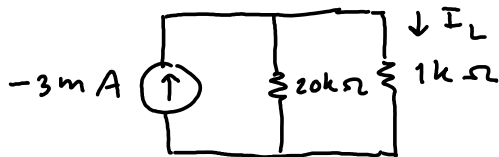
if I multiply these two equations by 1000, the m and k will magically disappear. So, I don't really have to care about them.

$$I_N = \frac{V_D}{10k} = \frac{-30}{10k} = -3mA$$

For R_N , we deactivate all the source and get



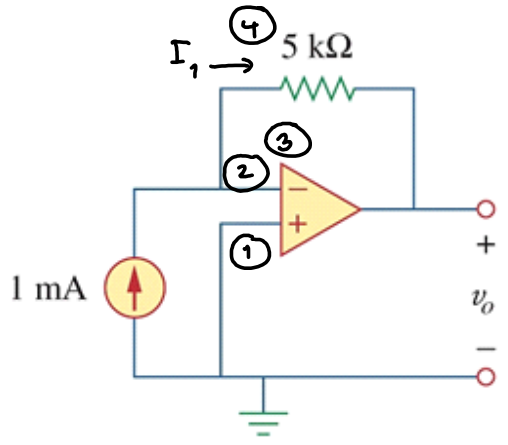
Now, we connect the Norton equivalent back to the load resistor:



The current I_L is $-3m \times \frac{1k}{\frac{1}{1k} + \frac{1}{20k}} = -3 \times \frac{20}{21} mA$

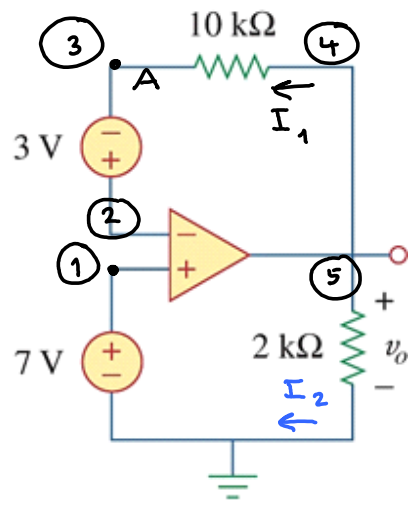
$V_o = I_L \times R_L = -3 \times \frac{20}{21} \times 1k = \boxed{-\frac{60}{21} V \approx -2.86 V}$

5.8



(a)

- ① $v_+ = 0\text{ V}$ because it is connected to the ground.
- ② $v_- = v_+ = 0\text{ V}$ by Rule #2
- ③ $i_- = 0\text{ A}$ by Rule #1
- ④ $I_1 = 1\text{ mA}$ because $i_- = 0$.
- ⑤ $v_o = v_- - I_1 \times 5\text{ k}$
 $= 0 - 1\text{ mA} \times 5\text{ k}\Omega$
 $= \boxed{-5\text{ V}}$



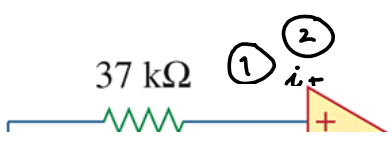
(b)

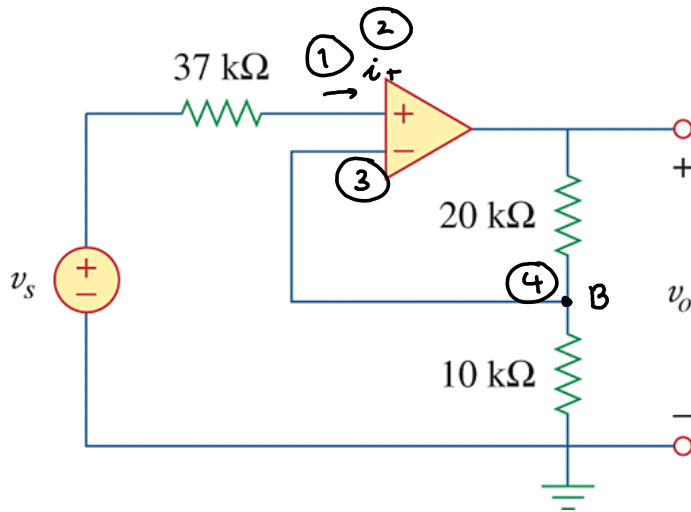
- ① $v_+ = 7\text{ V}$.
- ② $v_- = v_+ = 7\text{ V}$ by Rule #2.
- ③ $v_- - v_A = 3\text{ V}$
 $v_A = v_- - 3\text{ V}$
 $= 7\text{ V} - 3\text{ V}$
 $= 4\text{ V}$
- ④ $I_1 = i_- = 0$
by Rule #1
- ⑤ $v_o = v_A + I_1 \times 10\text{ k}$
 $= v_A + 0 = v_A$
 $= \boxed{4\text{ V}}$

Note: It is tempting to say $I_2 \approx i_+ = 0$ by Rule #1 and hence $v_o = 0 + I_2 \times 2\text{ k}\Omega = 0 + 0 = 0$

This is not true because there could be some current flows into the ground!!

5.10





- ① $i_+ = 0$ by Rule #1
- ② $v_+ = v_s - i_+ \times 37 \text{ k}\Omega = v_s - 0 = v_s$
- ③ $v_- = v_+ = v_s$ by Rule #2
- ④ KCL at B gives

$$\frac{v_B - v_o}{20 \text{ k}} + \frac{v_B}{10 \text{ k}} = 0$$

$v_B = v_- = v_s$ by ③

by Rule #1

$$\frac{v_B}{20 \text{ k}} + \frac{v_B}{10 \text{ k}} = \frac{v_o}{20 \text{ k}}$$

$$v_B + 2v_B = v_o$$

$$v_B = \frac{1}{3} v_o$$

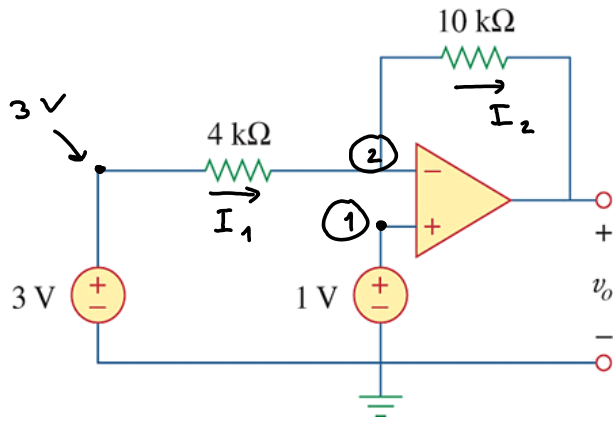
$$\therefore v_o = \frac{1}{3} v_s$$

$$\frac{v_o}{v_s} = 3$$

Alternatively, because $i_- = 0$, the relationship between v_B and v_o is given by voltage divider formula

$$v_B = \frac{10 \text{ k}}{20 \text{ k} + 10 \text{ k}} v_o$$

5.21



① $v_+ = 1V$

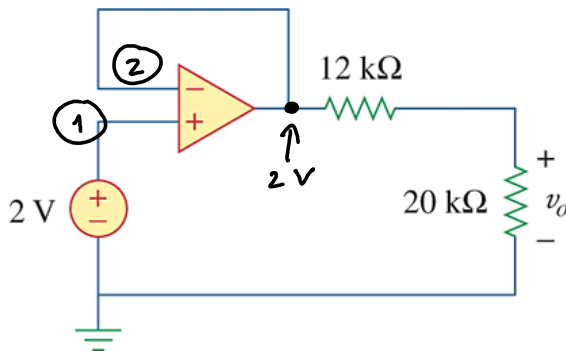
② $v_- = v_+ = 1V$

③ $I_1 = \frac{3 - v_-}{4k} = \frac{3 - 1}{4k} = \frac{1}{2} mA$

④ $I_2 = I_1$ because $i_- = 0$ by Rule #1.

⑤ $v_o = v_- - I_2 \times 10k = 1 - \frac{1}{2} mA \times 10k = \boxed{-4V}$

5.25



① $v_+ = 2V$

② $v_- = v_+ = 2V$ by Rule #2

③ By voltage divider formula,

$$v_o = \frac{20k}{12k + 20k} \times 2V = \frac{20}{32} \times 2 = \frac{40}{32} = \frac{5}{4} V = \boxed{1.25V}$$